

## THERMAL MODELING FOR ON-INTERPOSER THERMOELECTRIC SENSORS

COMSOL Conference Rotterdam | Morel Christophe & Savelli Guillaume



- Our aim is to design micro ThermoElectric Sensors (μTES) to detect hot spots in microelectronic devices.
- Use of the Seebeck effect which produces a voltage signal when the μTES is placed in a thermal gradient.

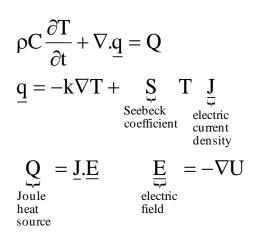
 A μTES is made of a large number of positive Seebeck coefficient lines (p-lines) connected to the same number of negative Seebeck coefficient lines (n-lines) to form p-n junctions.

- µTES are placed in-between a thermal test chip (TTC acting as a hot source) and a Si-based wafer which may be etched (or not) to integrate micro-channels for cooling by air or water
- The goal is to attain a sensitivity Se = 100 mV/°C with a short response time (< 400 ms).</li>

# THERMOELECTRICITY GOVERNING EQUATIONS (JAEGLE, 2007)

• Equation for the temperature T:

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• Electric current density (A/m<sub>2</sub>):

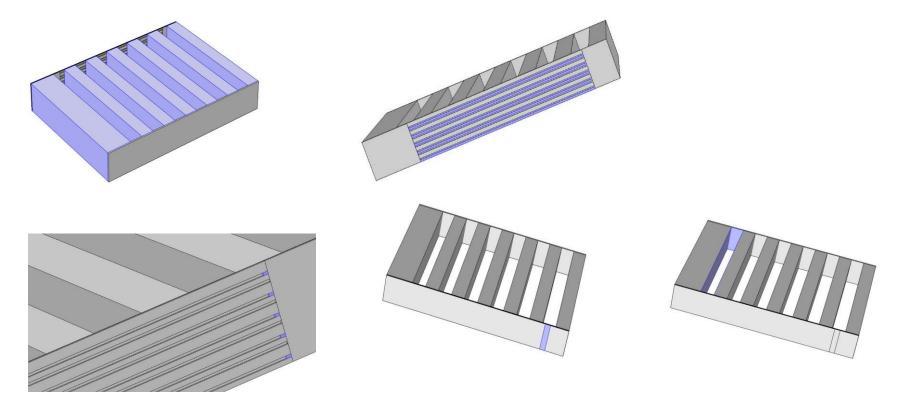
$$\underline{J} = - \underbrace{\sigma}_{\substack{\text{electrical}\\ \text{conductivity}}} \left( \nabla U + S \nabla T \right)$$

• Equation for the electric potential U (V):

$$\underbrace{\varepsilon}_{\text{permittivity}} \left[ \frac{\partial^2 U}{\partial x \partial t} + \frac{\partial^2 U}{\partial y \partial t} + \frac{\partial^2 U}{\partial z \partial t} \right] = -\nabla . \underline{J}$$

#### **Liten** GEOMETRICAL MODEL OF μTES AND MICRO-CHANNELS

- Only 5 junctions (10 lines) of the μTES are simulated (the complete μTES has 315 junctions which is not manageable by the simulation because of small details like silicides)
- Six micro-channels are simulated when they are present.





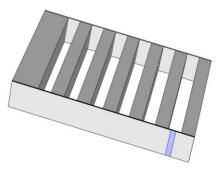
- Two different thermoelectric materials are tested: SiGe (Silicium Germanium alloy) and QDSL (Quantum Dot SuperLattices).
- Definition of parameters used

Materials	Si	Ge	QDSL		
Line type	р	n	р	n	
R = 1/σ (Ω.m)	3.10 <sup>-5</sup>	3,4.10 <sup>-5</sup>	1,6.10 <sup>-4</sup>	2,5.10-4	
S (mV/K)	142	-185	253	-267	
k (W/mK)	4.7	4.1	5.3	6.3	
ρ (kg/m³)	o (kg/m³) 2330		2330	2330	
C (J/kgK)	710	710	710	710	



We investigate two types of heat transfer boundary conditions:
-> Imposed temperature = 120 °C

-> Imposed flux density = P/S = 99469 W/m<sup>2</sup>

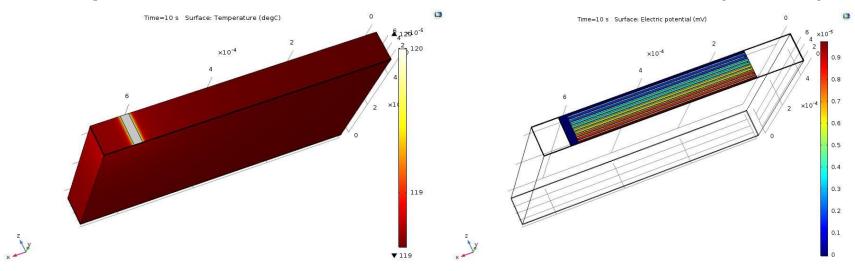


 Calculations with and without micro-channels are made in order to investigate the cooling effect.

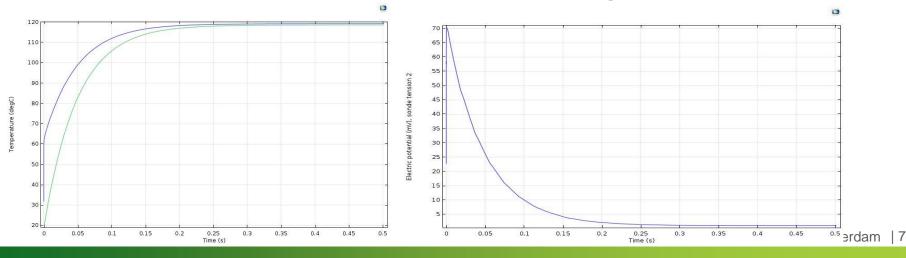
## IMPOSED TEMPERATURE WITHOUT MICRO-CHANNELS SIGE MATERIAL

• Temperature and electric fields at the end of the calc. (t = 10 s)

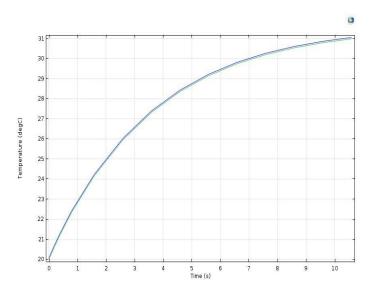
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Time evolution of the hot and cold sides temperatures and the U

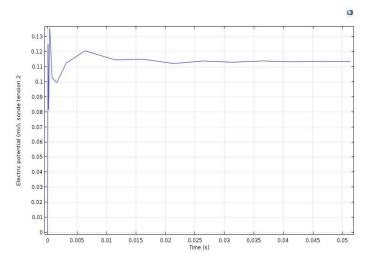


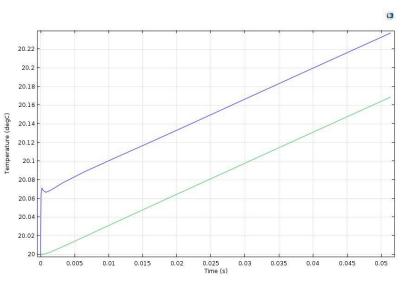
## IMPOSED FLUX WITHOUT MICRO-CHANNELS SIGE AND QDSL MATERIALS



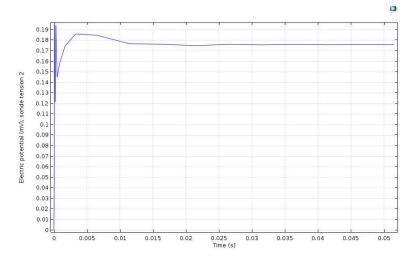
• Left: SiGe

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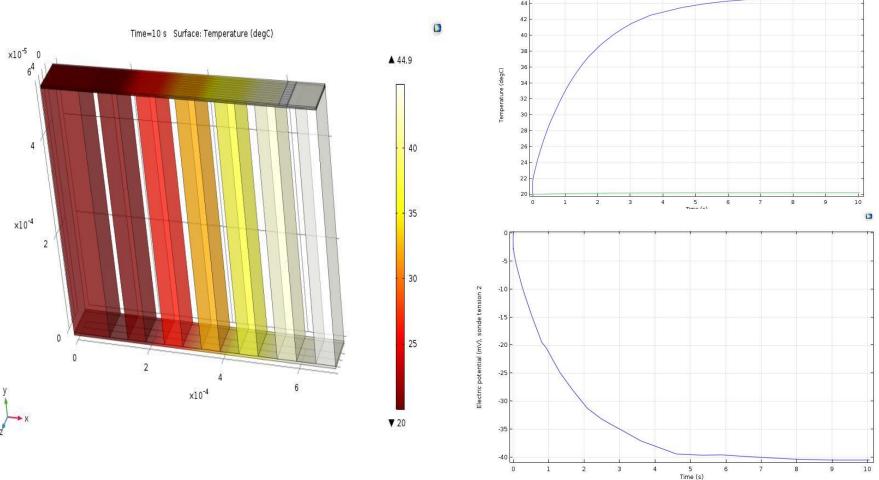






### Liten CERT OF THE CHANNELS SIGE AND IMPOSED HEAT FLUX

 5 micro-channels filled with air (h = 15 W/m<sup>2</sup>K) and 1 with water (h = 10000 W/m<sup>2</sup>K)



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#### Liten CALCULATION OF THE SENSITIVITY IN THE DIFFERENT CASES

Materials	heat transfer boundary conditions	µchannels	Temperature difference ΔT = Th – Tc (K)	Voltage U (mV)	Time t (s)	Sensitivity Se (mV/K) 5 junctions	Sensitivity Se (mV/K) 315 junctions
SiGe	120 °C	no	43	70	0.01 s	1.63	103
QDSL	120 °C	no	43	112	0.01 s	2.6	164
SiGe	flux	no	0.072	0.12	0.001	1.66	105
QDSL	flux	no	0.072	0.19	0.001	2.64	166
SiGe	flux	yes	25	41	5	1.64	103

- SiGe: 102.6 mV/K < Se < 105 mV/K for 315 junctions
- QDSL: 164 mV/K < Se < 166 mV/K for 315 junctions
- QDSL has a better performance due to its higher Seebeck coefficient



- The  $\mu\text{TES}$  sensitivities Se are always greater than the 100 mV/K required
- The response time varies with the temperature field predictions: a rapid temperature variation will give a quick response time





• EUROPEAN UNION

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#### Commissariat à l'énergie atomique et aux énergies alternatives 17 rue des Martyrs | 38054 Grenoble Cedex www-liten.cea.fr

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Établissement public à caractère industriel et commercial | RCS Paris B 775 685 019