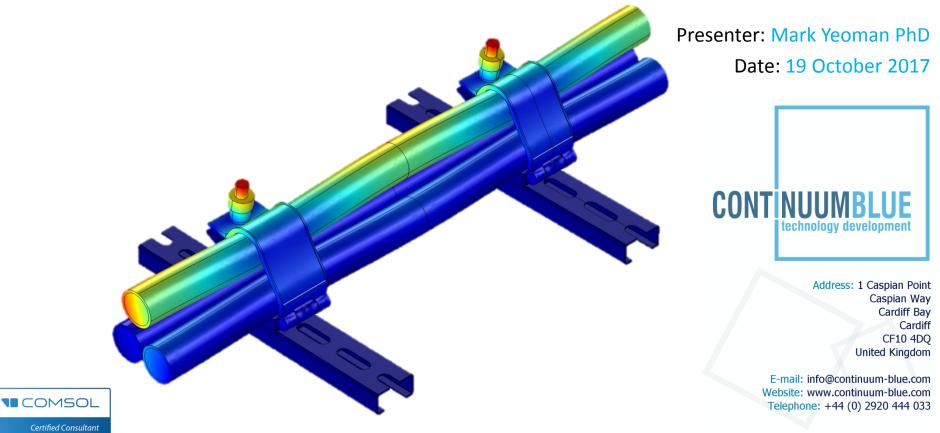
#### COMSOL CONFERENCE 2017 ROTTERDAM

## Multiphysics model to ensure power cables are restrained safely

M S Yeoman PhD<sup>1</sup>, R Damodharan<sup>1</sup>, R J Varley<sup>1</sup>, L Frizzell<sup>2</sup> 1. Continuum Blue Limited, One Caspian Point, Caspian Way, CF10 4DQ, United Kingdom 2. CMP Products Limited, 36 Nelson Way, Nelson Park East, Cramlington, NE23 1WH, United Kingdom



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## SINGLE PHASE CABLES

- Three phases, single core configurations:
  - Trefoil & Flat formation
- Minimises the induction of eddy currents
  - Reduce the effect of localised heating, while maintaining the current carrying capacity of the circuit
- Ideal for medium to high voltage cables
  - Up to 400kV

Unarmoured single core medium voltage cable (Draka Ltd. UK)



**Trefoil Formation** 



Flat Formation



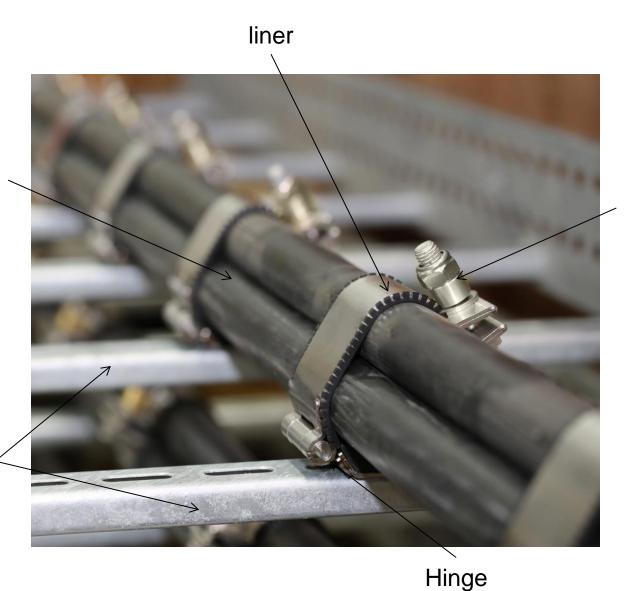


Short Circuit Failure Steel Cable Ties 42 kA / 100ms 36mm Ø Cables

## TREFOIL CLEAT DESIGNS IN USE

#### CURRENT: UP TO 200kA

Power cables in trefoil formation



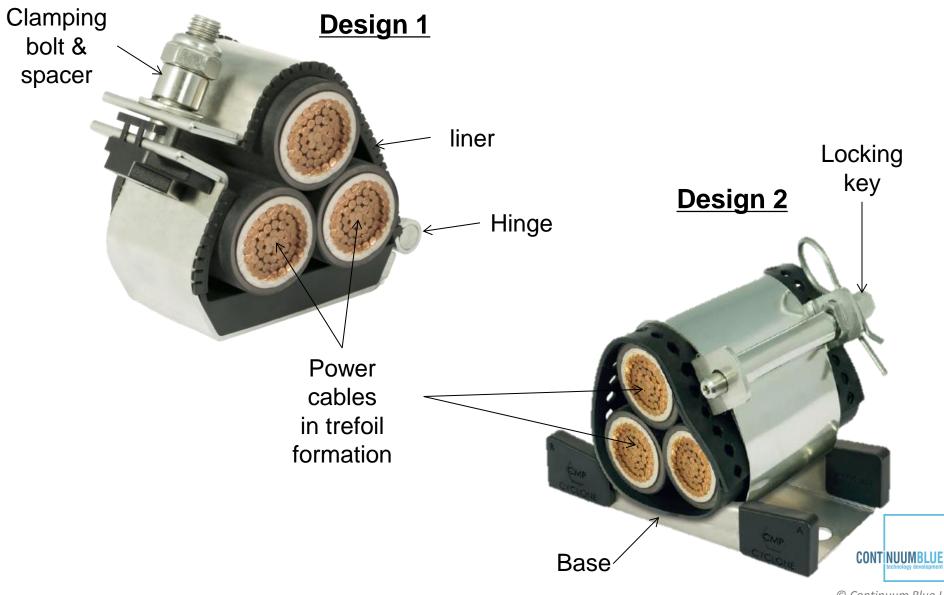
#### Clamping bolt & spacer

Attachment ladder fixed to wall/ceiling

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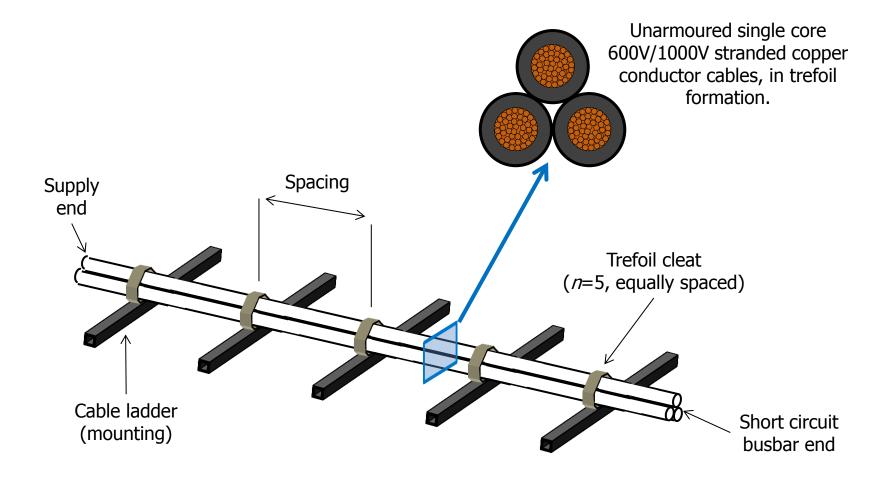
## EXAMPLE TREFOIL CLEAT DESIGNS

VARIOUS



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## TREFOIL TEST CONFIGURATION

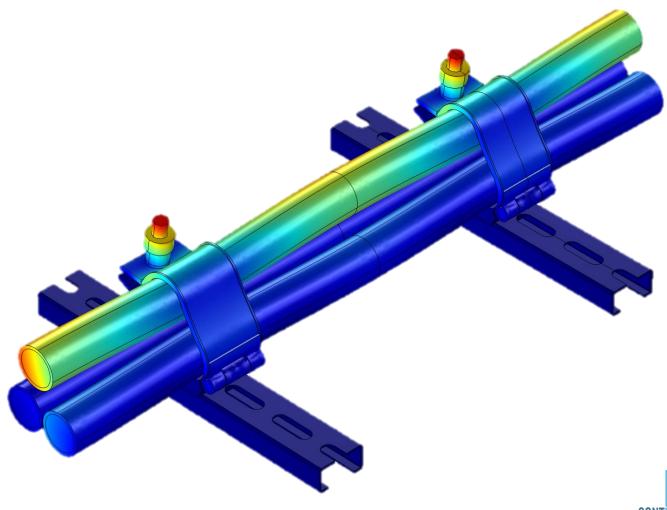




<u>Short Circuit Pass</u> <u>Steel Cleats</u> 190 kA / 1000ms 36mm Ø Cables Standard (IEC 61914:2015)

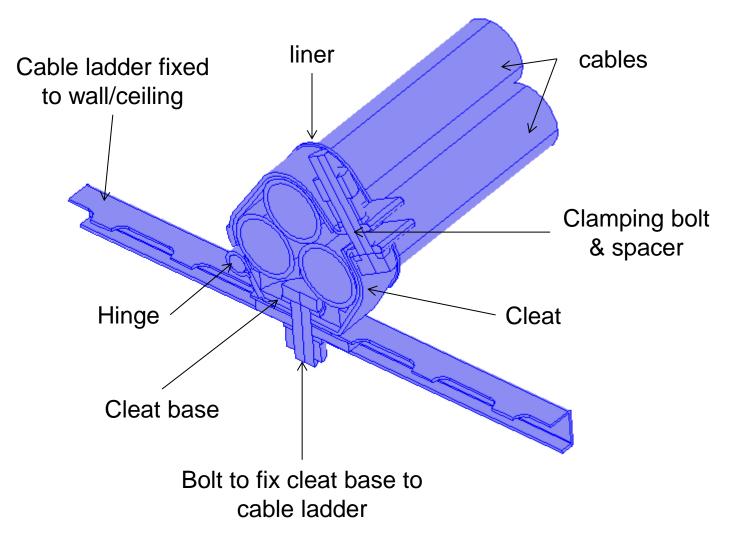
- $\rightarrow$  Not necessary for manufacturer of cleats to test product to standards
- $\rightarrow$  Test setup allows discretion of user to change/adjust ladder, ladder mountings & bolts.
  - Stiffer ladder & ladder mountings can change results drastically
  - Different size bolts & bolt specifications including torque loading can pass/fail cleat design
- $\rightarrow$  Orientation of cleats can be at users discretion
  - For single bolt systems, bolt can be placed on either side depending on user preference
- $\rightarrow$  Certification by 3rd party
  - Only requires inspection & observation of physical test
  - Pass/fail for grade







## COMPONENTS MODELLED



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## LOAD CONDITIONS & INSTALL CONFIGURATION

Cleat type: Cleat Configuration: Cable diameter: Cable Core Area: Cleat spacing: Peak fault current:

٠

Design 1 33-38 36 mm 500 mm<sup>2</sup> 300 mm 190 kA



MODEL



## COUPLED PHYSICS & BOUNDARY CONDITIONS

**Structural Mechanics** 

- Hyperelastic Material  $\rightarrow$  Sheath
- Plasticity  $\rightarrow$  Copper Cores
- Contact Mechanics  $\rightarrow$  Cables/Cleat

Coupled Physics & Mathematics

& Boundary Conditions Electrical (AC)

- $AC \rightarrow Copper Cores$
- Current density applied

Magnetic

- Magnetic field (B)
- Lorentz Forces

Moving mesh

Updating cable positions

Ladder ends fully constrained

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MODEL

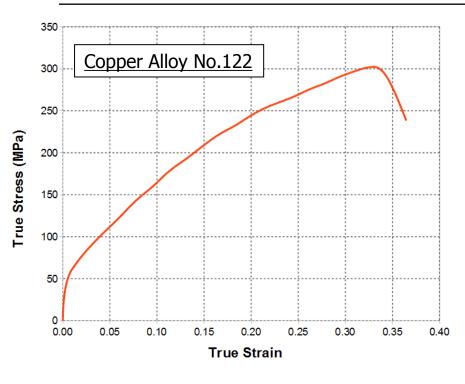
Symmetry & periodic conditions

appropriate

## MATERIAL RELATIONS



- Polyurethane Sheath
- Material Models  $\rightarrow$  Elasto-plastic Materials
  - Cable Cores •
  - Copper Alloy No.122 •
  - **Stainless Steel Cleat** •

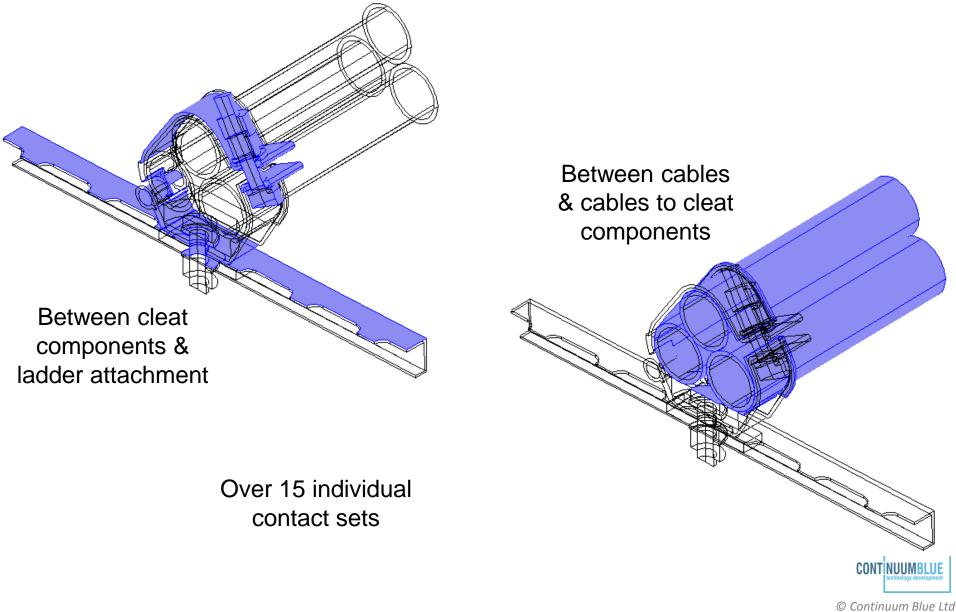


Stainless Steel **Mechanical Properties** (Utilized Minimum value in range)

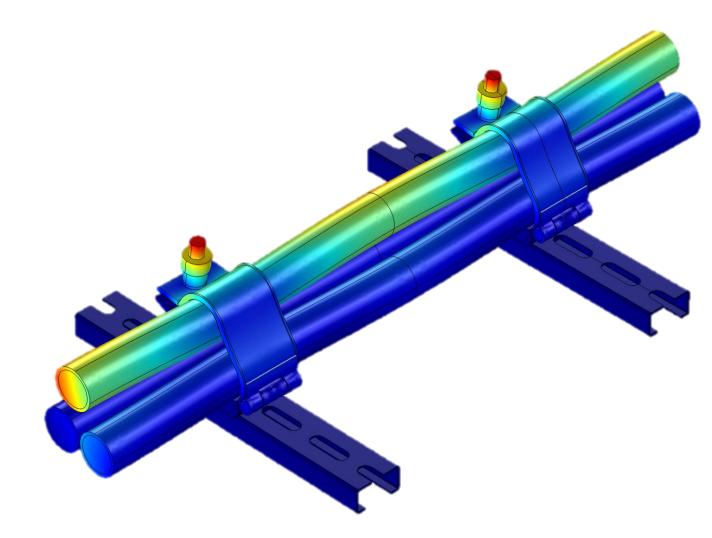
Young's modulus	190	-	203	GPa
Flexural modulus	190	-	203	GPa
Shear modulus	74	-	81	GPa
Bulk modulus	134	-	151	GPa
Poisson's ratio	0.265	-	0.275	
Shape factor	62			
Yield strength (elastic limit)	205	-	310	MPa
Tensile strength	510	-	620	MPa



## CONTACT



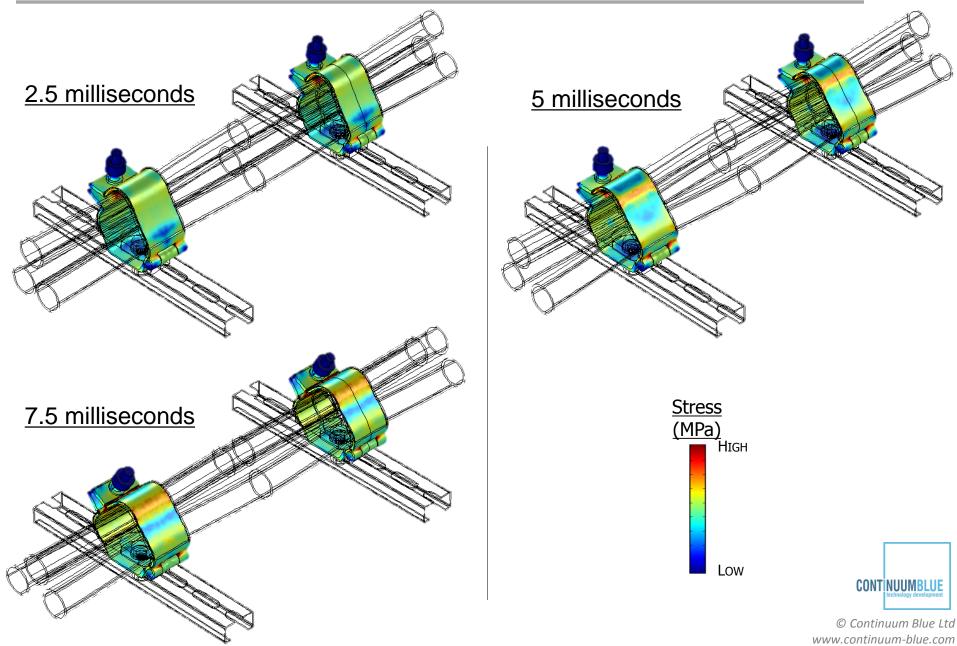
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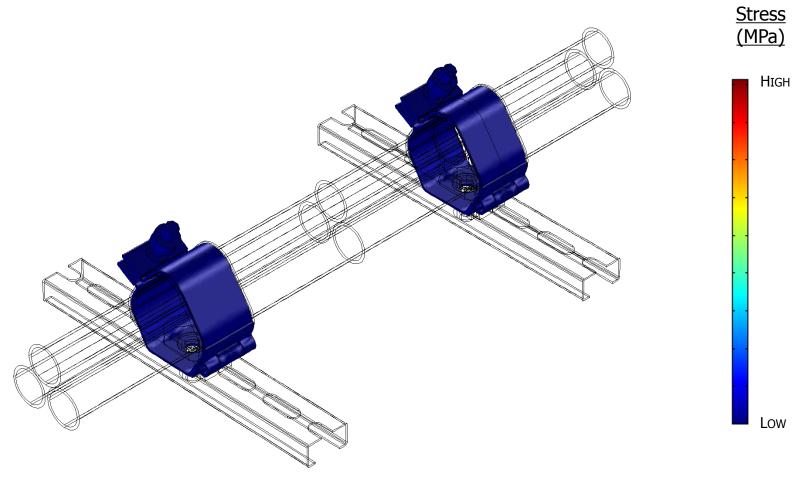


## CLEAT STRESSES

**DURING SHORT-CIRCUIT** 



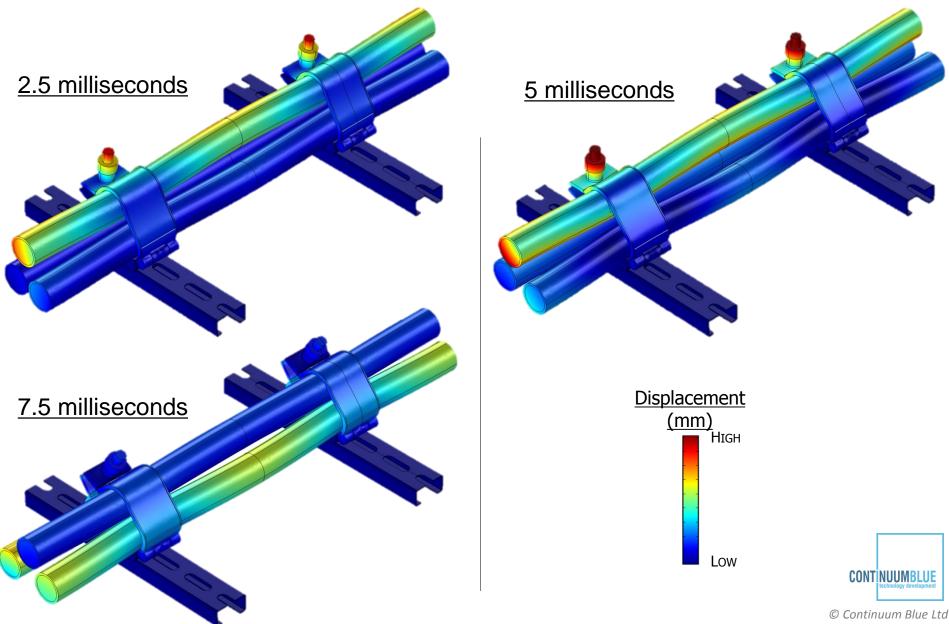
## **CLEAT STRESSES**





## CABLE & CLEAT DISPLACEMENTS

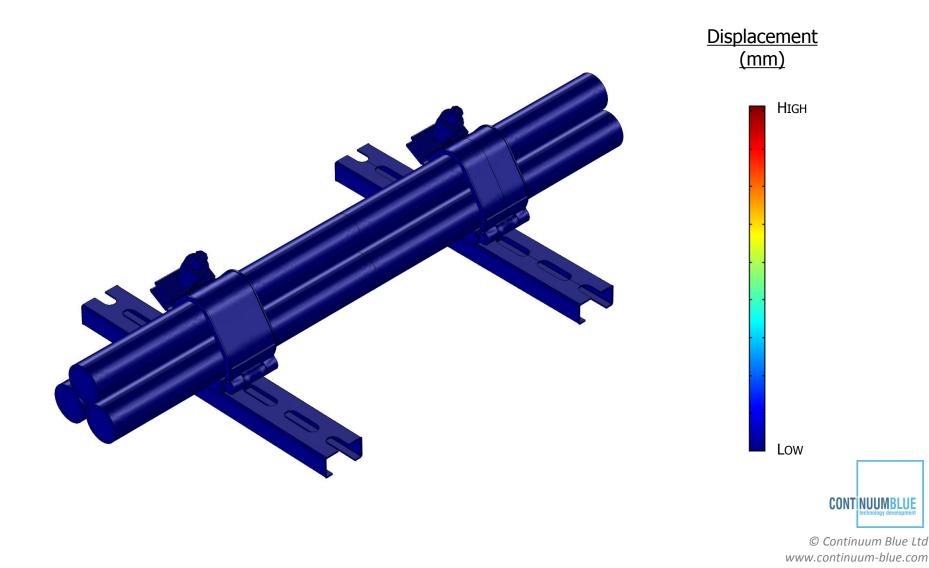
#### **DURING SHORT-CIRCUIT**



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## CABLE & CLEAT DISPLACEMENTS

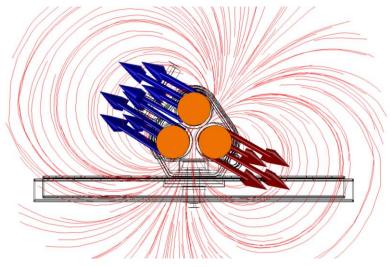
**ANIMATION** 

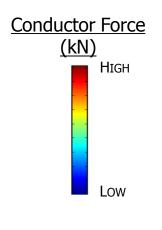


## FORCE VECTORS & MAGNETIC FIELD DURING SHORT-CIRCUIT

# 2.5 milliseconds 7.5 milliseconds

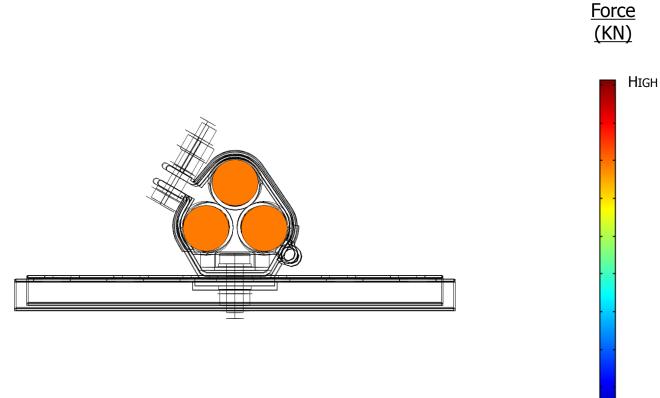
#### 5 milliseconds





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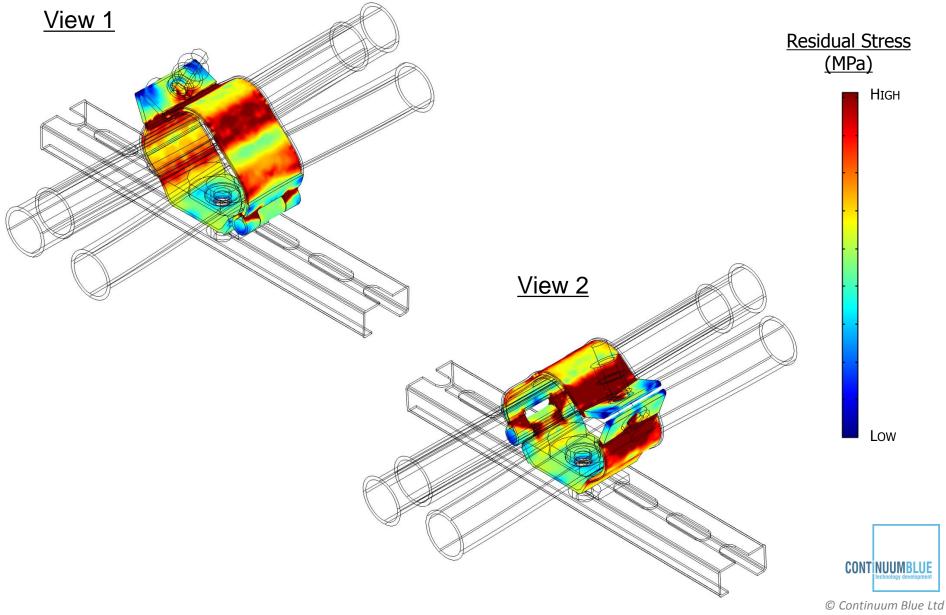
## Force Vectors & Magnetic Field



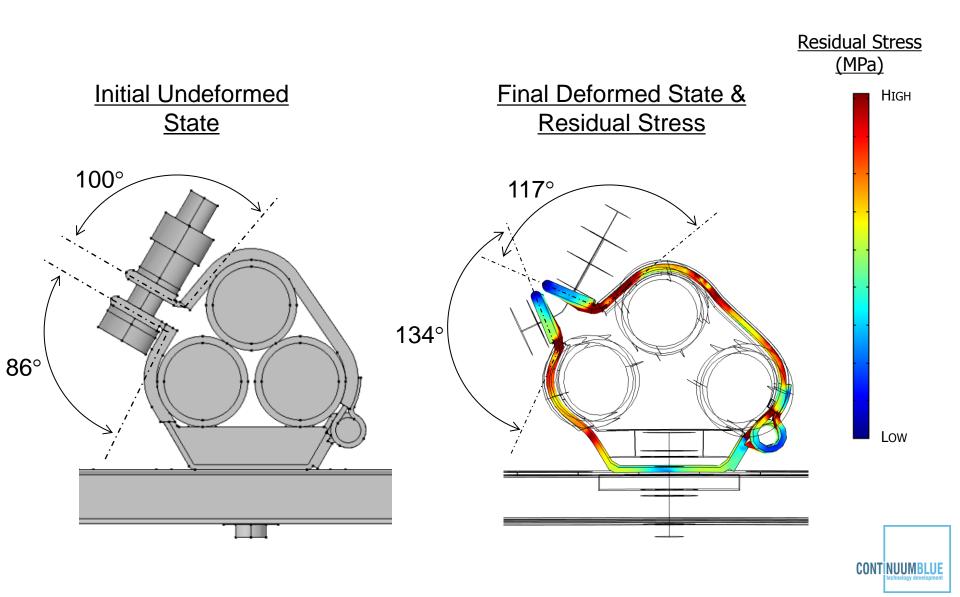
Low



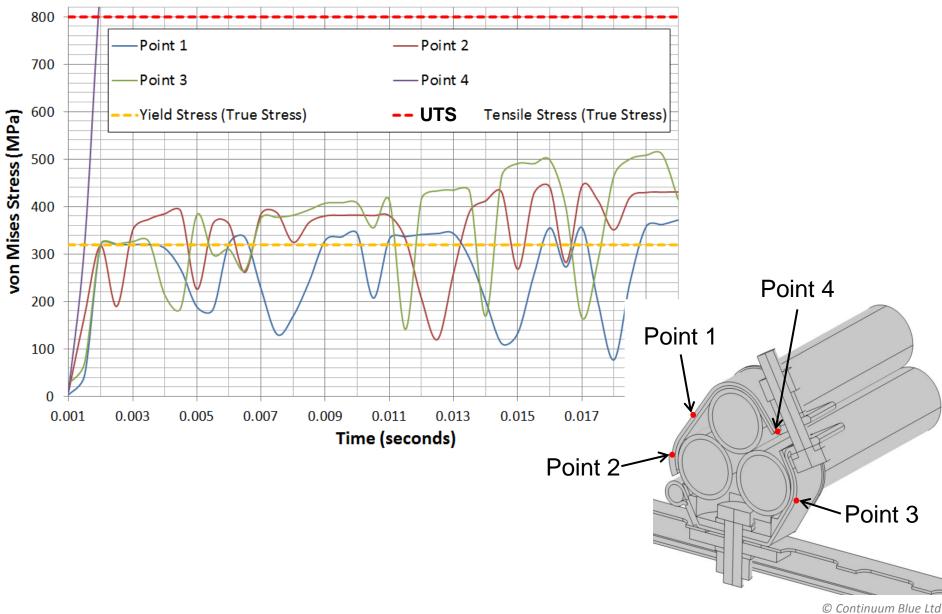
## RESIDUAL STRESSES IN CLEAT



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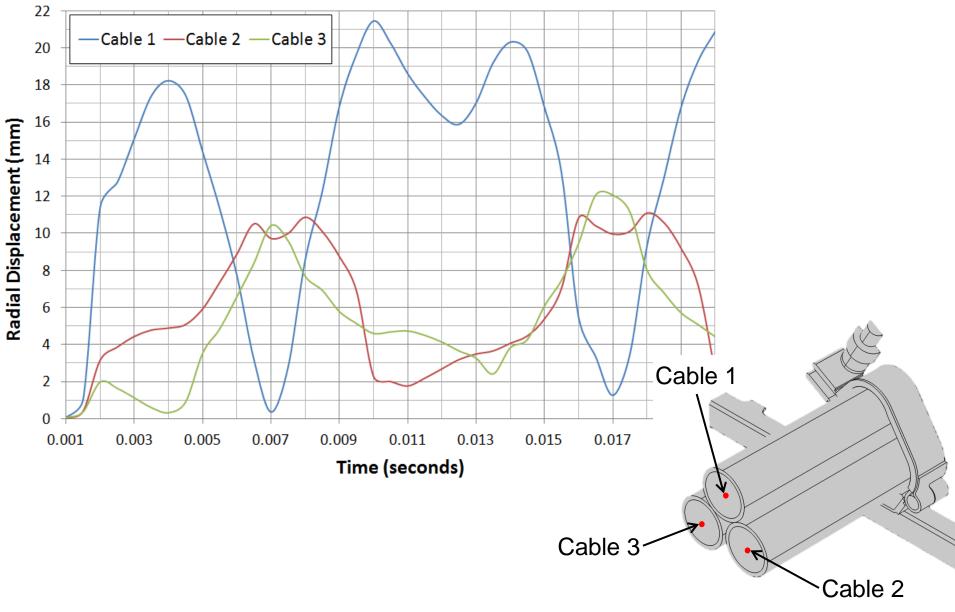
## STRESS ANALYSIS AT SPECIFIC POINTS

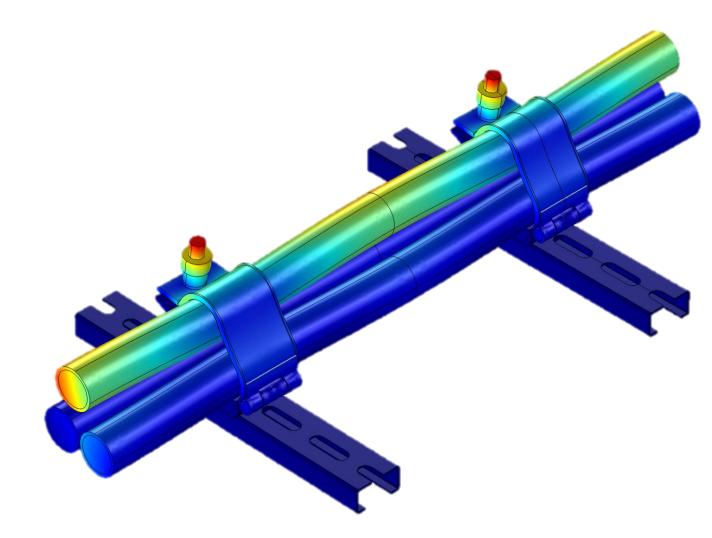


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## CABLE DISPLACEMENTS

#### **DURING SHORT-CIRCUIT**





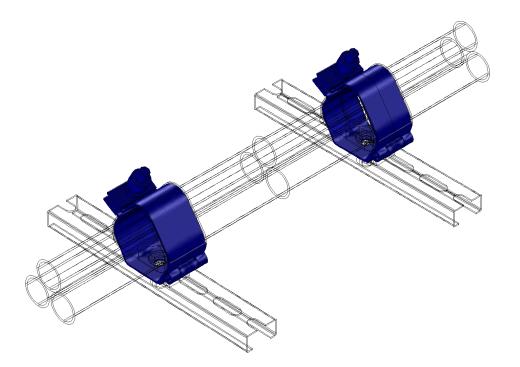


## COMPARISON TO PHYSICAL TESTS

Physical Test

Model (Cleat von Mises Stress)







## VALIDATION

#### VARIOUS TIME POINTS

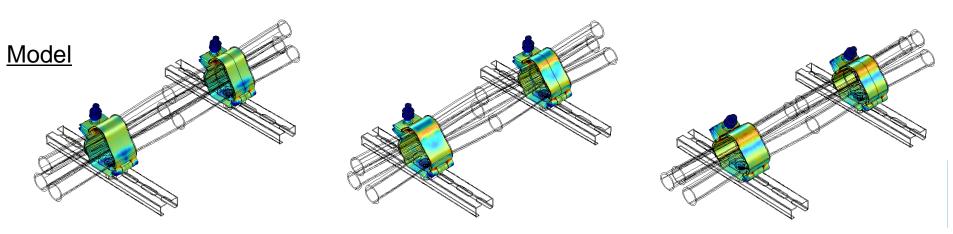
#### 2.5 milliseconds

#### 5 milliseconds

#### 7.5 milliseconds

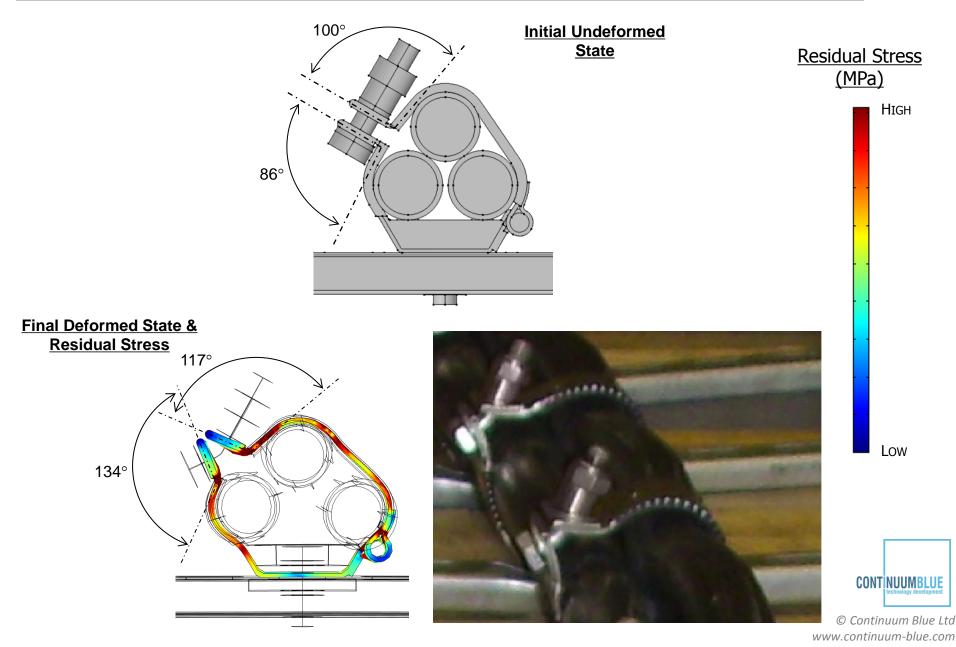
#### Physical Test





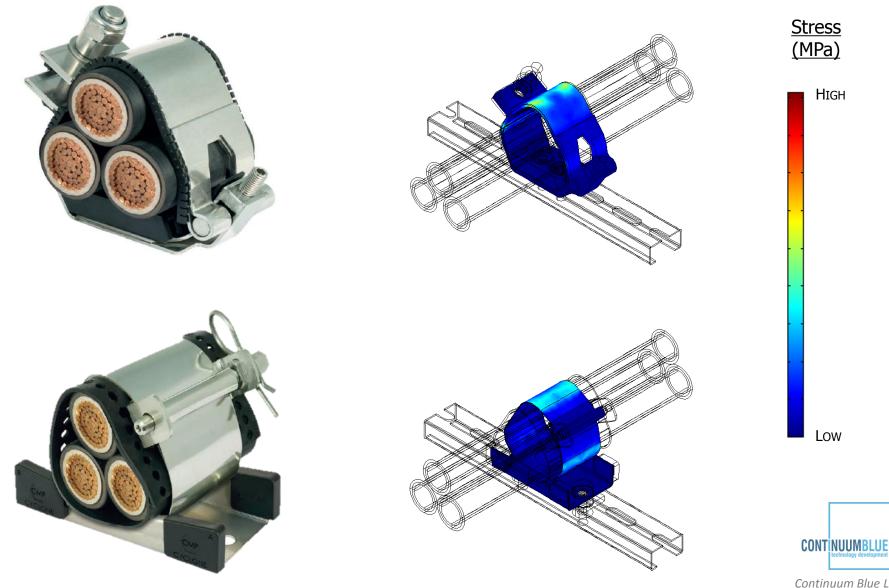
## VALIDATION

#### PERMANENT DEFORMATION & RESIDUAL STRESS



## **OTHER CLEAT DESIGNS & PHYSICAL TESTS**

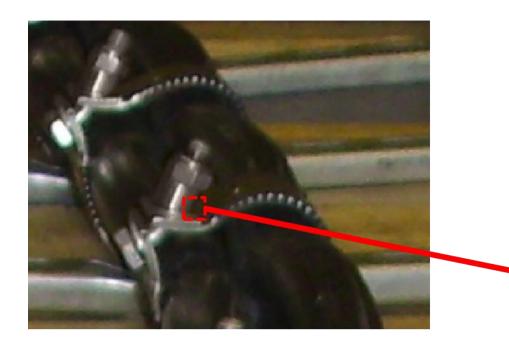
#### CORRELATIONS



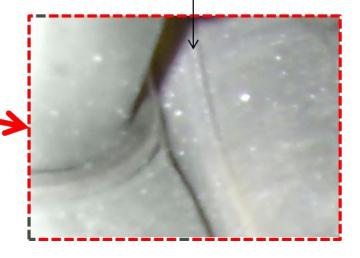
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## SUPERFICIAL SURFACE MATERIAL FAILURE

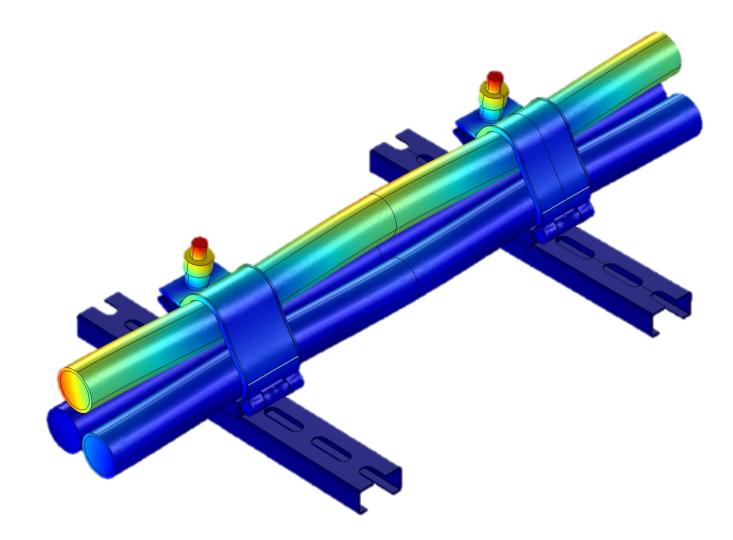
ABOVE UTS



Small amounts of micro-cracking on top surface of cleat wall at crease/bend









A three-phase short circuit in trefoil formation, the maximum force on the conductor as detailed in IEC 61914:2015 (Appendix B), is described by the following:

$$F_t = \frac{0.17 \times i_p^2}{S}$$

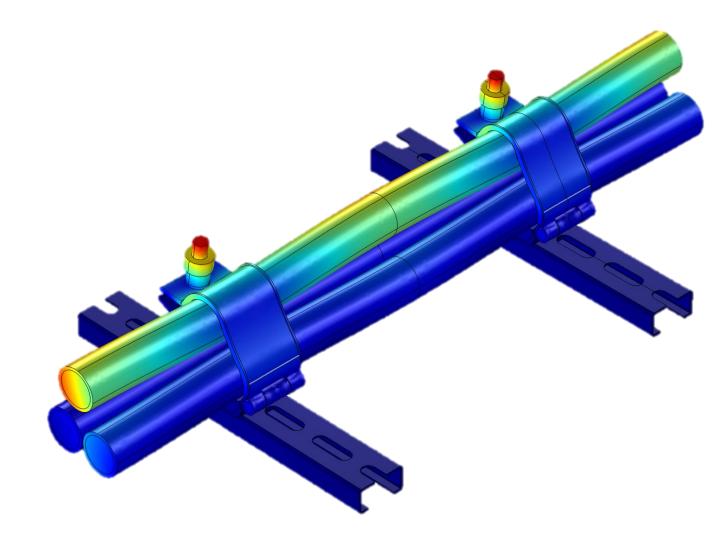
Where:

- $F_t$  Maximum Force per unit length of cable (N/m)
- $i_p$  Peak short circuit current (kA)
- S Centre-to-centre distance between neighbouring conductors (m)



#### Maximum force per unit cable length

IEC 61914 Standard	Model Results		
$F_t = \frac{0.17 \times i_p^2}{S}$ Parameters: S= 36mm $i_p = 190$ kA	Cable section constrained within cleat width only	Along whole length of cable, including cable length between adjacent cleats	
170.5 kN/m	159.3 kN/m	124.5 kN/m	
Percentage Variation	-6.53%	-26.98%	





## CONCLUSION

 A 3D multiphysics model has been developed, which is fully parameterised and couples the electrical, magnetic and structural physics to fully describe the response of a constraining cleat under short-circuit conditions.



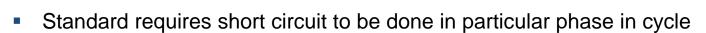
Design 3

- The multiphysics model has been assessed & compared to physical tests for a range of cleat designs, sizes & spacing.
- The multiphysics model provides additional data for design engineers, which would not be possible to gain through physical tests. Additionally, this can provide data such as residual stresses within the cleat, which is not physically possible, without destroying the cleat in the process.
- The models maximum force per unit length observed by the short-circuiting cables has also been assessed & compared to the analytical solution from the IEC 61914:2015 standard, where the model predicts a value 6.53% lower to the analytical solution.
  - This is expected as the model takes into account movements of the cables within the cleat, & the resulting reduction in the electromagnetic forces.

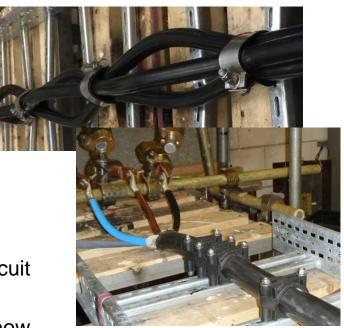


## DISCUSSION

- Much work still needs to be done on the multiphysics model, including further additions;
  - Intermediate straps,
  - Additional cable options, such as cable armour sheath material options.
  - Assessment of Category 2, or multiple short-circuit testing.
  - The possibility of two phase short-circuit faults, and how this may change the cleat performance.



- Thus, initial position of side bolt position: left vs. right will affect failure outcome
- Standard needs to be updated to ensure test is carried out with side bolts positions alternated along length of ladder
- Test standard does not specify which cable copper alloy is to be used, only that cable must not have an armour layer
  - Copper alloys with low stiffness & yield point gives dramatically better results





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## **Questions & Answers**

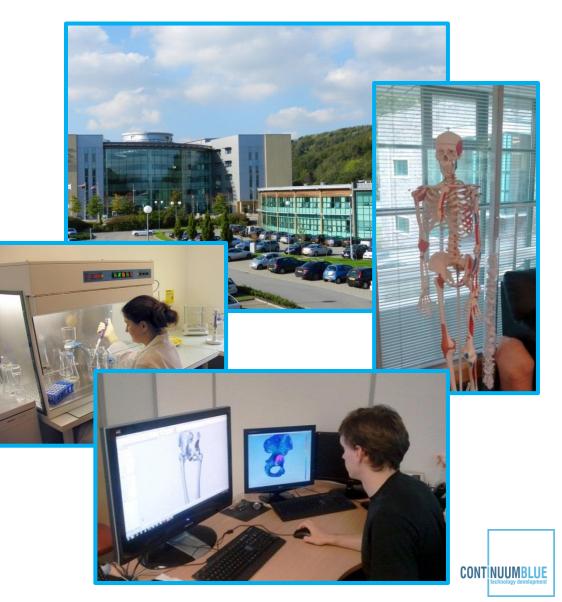


#### Research & Development

Multiphysics Modeling (FEA/CFD) Motion & Load Analysis Material Selection & Optimization

#### Testing & Assessment

Mechanical Testing Material Assessment



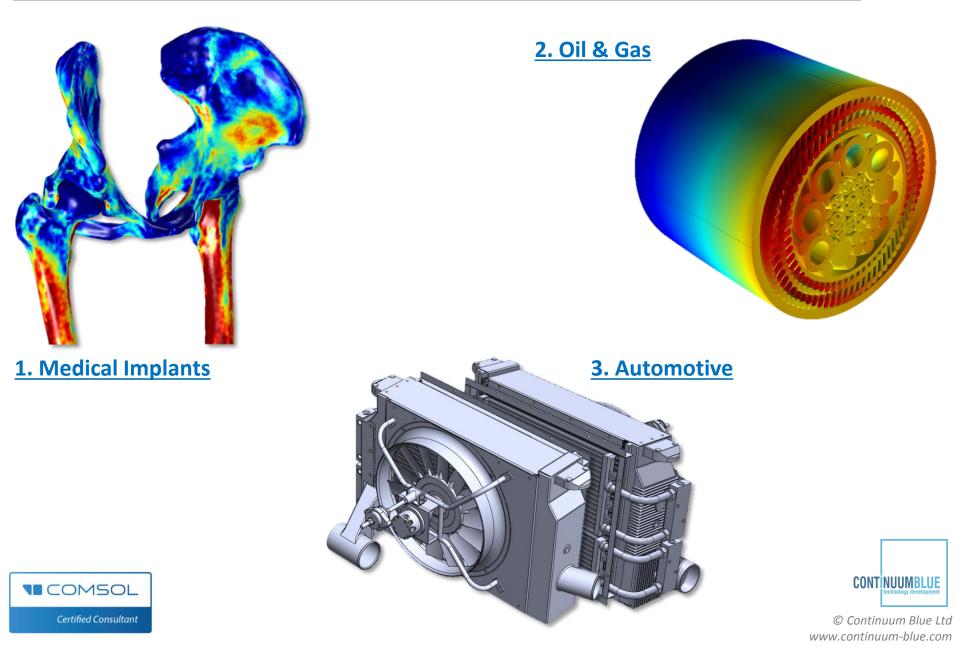


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**OVERVIEW** 

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#### STRUCTURAL PROJECTS



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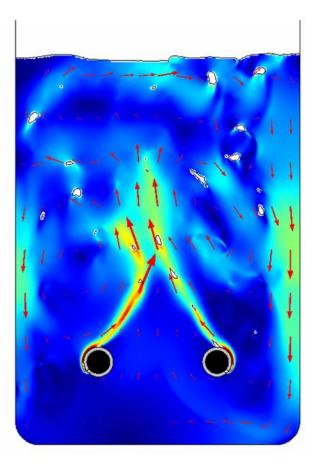
#### FLUID FLOW PROJECTS





Image courtesy: Alchemy Pharmatech Ltd.

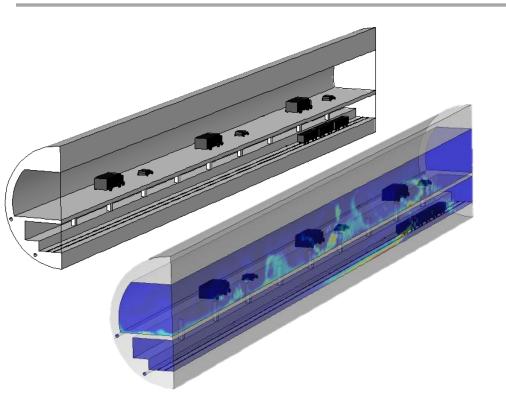




#### **2. Bioreactors**



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#### 3. Transport

- Vehicle emissions in tunnel
  - Air quality analysis

#### 4. Mould Flow Analysis

- Multiphase flow
- Mixing of Polymers
  - Thermal
  - Polymer curing

